

Original Article

# Bandwidth and Return Loss Improvement Technique Using Double-Material Substrate Cylindrical Surrounding Patch Antenna:Part-I

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**Abstract** - For the purpose of bandwidth enhancement, return loss improvement, and providing a solution to the negative effect of dimension inaccuracy, a Double Material Substrate (DMS) antenna composed of FR-4 (lossy), polyimide (lossy), and a partial ground plane of copper (annealed) has been presented in this work. The proposed antenna has been compared with a Single Material Substrate (SMS) antenna composed of FR-4 (lossy) and a partial ground plane of copper (annealed). Findings reveal that the cylindrical conformal antennas designed with DMS are significantly better in terms of bandwidth and return loss. The antenna with SMS presented a return loss and bandwidth value of -27 dB and 0.783 GHz (1962 MHz ~ 2745MHz), respectively, at a resonance frequency of 2.4 GHz. Also, at the same resonance frequency, the DMS antenna presented an enhanced return loss and bandwidth of -35.2 dB and 0.862 GHz (1844 MHz ~ 2700 MHz), respectively.

**Keywords** — Bandwidth, Returns Loss, WiMAX, WLAN, Cylindrical Surrounding Patch Antenna (CSPA).

## I. INTRODUCTION

Due to the lightweight, easy fabrication process, feeding techniques flexibility, implementation, and radiation properties. Capitalizing on these advantages, researchers have made different forms and dimensions of microstrip patch antennas for use in wireless communication systems [1]-[4]. One of such forms of the microstrip patch antenna is the Cylindrical Surrounding micro-strip fed Patch Antenna (CSPA). This form of antenna has been observed to have a better performance when compared with the regular rectangular patch antenna [2], [4].

Even though cylindrical surrounding patch antennas provide a series of advantages, they also have certain drawbacks, such as limited bandwidth, low gain, high return loss, and deteriorated radiation pattern. However, various researchers have used a variety of techniques to address challenges of limited bandwidth, high Return Loss ( $S_{11}$ ) and, poor radiation pattern [5]-[8]. For the purpose of bandwidth enhancement of microstrip patch antenna, a Defected Ground

Structure (DGS) consisting of an I-shape slot in the ground was presented by Singh et. al.[9]. Parameters such as bandwidth, return loss, and Voltage Standing Wave Ratio (VSWR) were much improved in the designed antenna than simple MPA without defected ground structure. The designed antenna was observed to resonate in the C-band at a frequency of 6.0718 GHz with a bandwidth of 132.3 MHz and a very good return loss of -46.75 dB.

In this present research work, bandwidth and return loss enhancement techniques have been analyzed. Also, this technique serves as a solution to the negative effects of inaccuracy in dimension resulting from the reduced size of antenna fabricated at high frequency using high dielectric permittivity materials.

To solve dimension inaccuracy during the fabrication process, a CSPA design with Double Material (DM) was proposed by Omoru and Srivastava[10]-[12]. However, the presented DMS antenna designs could suffer from phase impedance and resonance frequency errors resulting from mechanical tension effects (caused by compression and stretching of the dielectric substrates). The proposed antenna is also a solution to device fitting issues currently being experienced by mobile device design engineers. Thereafter, the proposed DMS CPA has been compared with SMS CPA using the 2.4 GHz band. This paper has been structured as follows. Section II has an overview of DMS and SMS cylindrical patch antenna. Section III realized the performance analysis of DMS and SMS CSPA. Section IV gives a comparative analysis of DMS and SMS antennas. Finally, Section V concludes the work and recommends the future aspect.

## II. OVERVIEW OF DMS AND SMS CYLINDRICAL PATCH ANTENNA

Most of the antenna design parameters are dependent on the effective dielectric constant of substrate materials used[13]-[15]. Here the effective dielectric constant has been computed as a function of the resultant dielectric constant of the two substrate materials used FR-4 ( $\epsilon_{r,fr-4}$ ) and dielectric constant for having polyimide ( $\epsilon_{r,pi}$ ) as shown in Eq. (1) to Eq. (3). A design frequency of 2.4 GHz has been adopted for



the modeling of the proposed antenna. The values for  $\epsilon_{r,fr-4}$  and  $\epsilon_{r,pl}$  are 4.3 and 3.5, respectively:

$$\epsilon_{R,r} = \frac{\epsilon_{r,fr-4} + \epsilon_{r,pl}}{2} \quad (1)$$

$$W_p = \frac{V_0}{2F_r} \sqrt{\frac{2}{\epsilon_{R,r}}} \quad (2)$$

From Eq. (1) and Eq. (2), the resultant dielectric constant and width of the patch have been calculated as 3.9 and 29.96 mm, respectively. Also, the thickness of polyimide ( $H_{s,pl}$ ), thickness of FR-4 ( $H_{s,fr-4}$ ), height of the patch ( $H_p$ ), height of the ground have been chosen as 2.0 mm, 2.8 mm, 0.8mm, and 0.8 mm, respectively[16]-[18]. Substituting these values into Eq. (3), the effective resultant dielectric  $\epsilon_{r,eff}$  substrate has been calculated as 3.3.

$$\epsilon_{r,eff} = \frac{\epsilon_{R,r} + 1}{2} - \frac{\epsilon_{R,r} - 1}{2} \left( 1 + \frac{12(H_{s,pl} + H_{s,fr-4})}{W_p} \right) \quad (3)$$

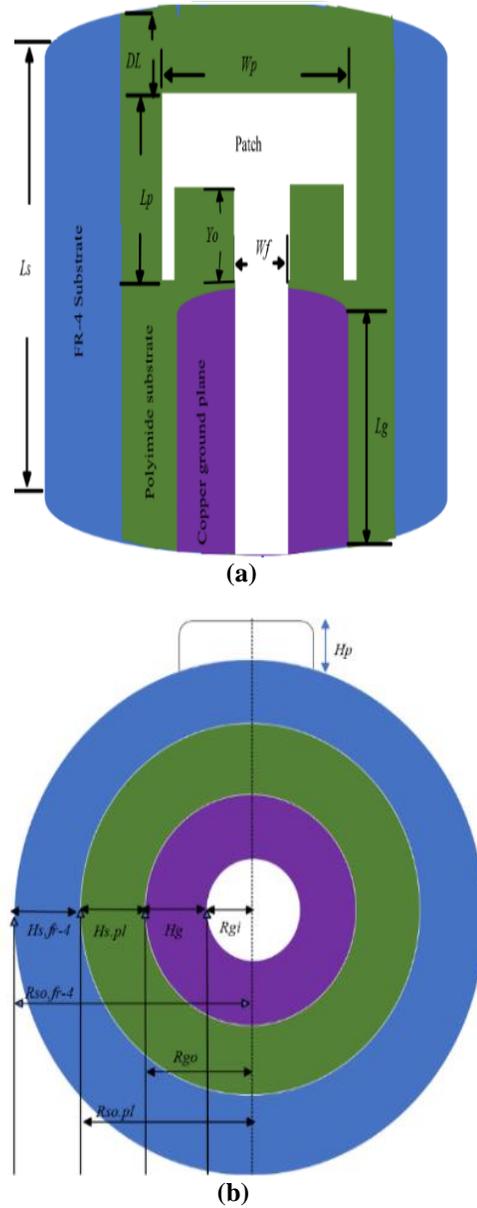
Using equations presented in [19]-[21] and known values of  $\epsilon_{R,r}$ ,  $\epsilon_{r,eff}$ , and  $W_p$ , other antenna design parameters have been calculated and recorded in Table I.

**TABLE I.**  
**DMS CSPA DESIGN PARAMETERS**

| Nomenclature                            | Symbol        | Value (mm) |
|---|---------------|------------|
| The outer radius of ground              | $R_{go}$      | 13.4       |
| Inner radius of ground                  | $R_{gi}$      | 14.2       |
| The outer radius of polyimide substrate | $R_{so,pl}$   | 16.2       |
| Outer radius of FR-4 substrate          | $R_{so,fr-4}$ | 19.0       |
| Length of ground                        | $L_g$         | 26.64      |
| Length of substrate                     | $L_s$         | 50.28.     |
| Substrate and patch top difference      | $\Delta L$    | 2.2        |
| Inset feed length                       | $Y_o$         | 7.0        |

Using parameters in Table I, three distinct techniques have been used to produce the proposed Dual-Material Substrate (DMS) Cylindrical Surrounding Patch Antenna (CSPA) design, as shown in Fig. 1. At first, using the electronic device simulator, a partly cylindrical copper ground plane with length ( $L_g$ ), inner radius ( $R_{gi}$ ), and outer radius ( $R_{go}$ ) was initially created. Secondly, a cylindrical substrate composed of polyimide material of length ( $L_s$ ),

thickness ( $H_{s,pl}$ ), and outer radius ( $R_{so,pl}$ ) was constructed on the cylindrical copper ground plane. Also, on the first cylindrical substrate, an outer cylindrical substrate made of FR-4 material with length ( $L_s$ ), thickness ( $H_{s,fr-4}$ ), and outer radius ( $R_{so,fr-4}$ ) was constructed. Finally, a copper patch of width ( $W_p$ ) and length ( $L_p$ ) was constructed and bent around the outer cylindrical substrate using the simulator bending functionality, thus providing a fully parameterized DMS CSPA conformal cylindrical patch antenna. A full design procedure, analysis, and mathematical modeling of the proposed DMS CSPA are presented in ref. [10].



**Fig. 1. Proposed DMS cylindrical surrounding patch antenna (a) front view and (b) bottom view [10].**

**TABLE II**

**SMS CSPA DESIGN PARAMETERS**

| Nomenclature                       | Symbol     | Value (mm) |
|------------------------------------|------------|------------|
| The outer radius of ground         | $R_{go}$   | 13.9       |
| The inner radius of ground         | $R_{gi}$   | 13.2       |
| The outer radius of FR-4 Substrate | $R$        | 18.8       |
| Thickness of substrate             | $H_s$      | 4.8        |
| Thickness of ground                | $H_g$      | 0.8        |
| Width of feed                      | $W_f$      | 7.5        |
| Width of patch                     | $W_p$      | 28.8       |
| Width of ground                    | $W_g$      | 59.6       |
| Thickness of patch                 | $H_p$      | 0.8        |
| Length of ground                   | $L_g$      | 26.6       |
| Length of substrate                | $L_s$      | 49.0       |
| Substrate and patch top difference | $\Delta L$ | 2.1        |
| Inset feed length                  | $Y_o$      | 7.0        |

Similar design procedures have been adopted for the SMS CSPA and equations from the research work of Umayah and Srivastava [22], [23], have been used to calculate the design parameters of the SMS antenna. The SMS cylindrical surrounding patch antenna consists of a metallic radiating element (copper) conformed on a cylindrical dielectric FR-4 substrate and a partial metallic ground (copper) inside of the cylindrical substrate. The SMS and DMS antennas have been fed using a microstrip line feeding technology to easily integrate with other components. Unlike coaxial feed, which provides its feeding from below the patch [24]-[26].

**III. PERFORMANCE ANALYSIS OF PROPOSED DMS CSPA AND SMS CSPA**

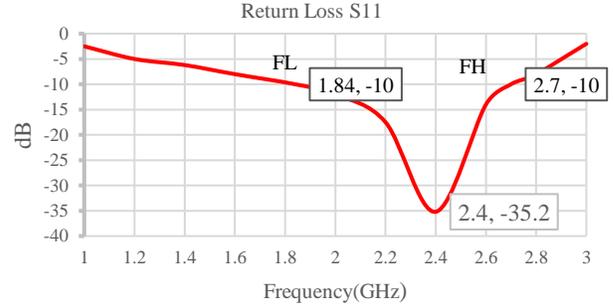
The microstrip antenna conformed on a cylindrical structure is shown in Table 3. The DMS CSPA performance parameters DMS and SMS surfaces with a microstrip feed have been simulated and performance analysis of both antennas is explained based on return loss and bandwidth. The simulated bandwidth and return loss characteristics of the proposed microstrip antenna conformed on cylindrical DMS, and SMS surface have been observed as -35.2 dB and -27.5 dB as illustrated in Fig. 2(a) and Fig. 2(b), respectively.

From the return loss plots, the bandwidth of the proposed design and SMS antenna has been calculated as 0.86 GHz. and 0.76 GHz, respectively. Also, percentage bandwidth for DMS and SMS antenna design have been calculated using the equation in [27],[28], and values have been recorded in Table III and Table IV, respectively:

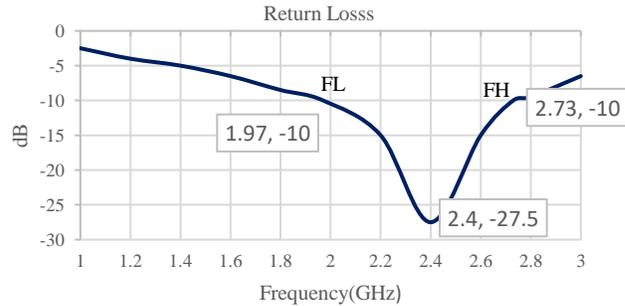
$$F_C = \frac{F_H + F_L}{2} \tag{4}$$

$$\% \text{ Bandwidth} = \frac{F_H - F_L}{F_C} \times 100 \tag{5}$$

where  $F_H$ ,  $F_L$ , and  $F_C$  are the highest, lowest, and center frequency, respectively.



(a)



(b)

**Fig. 2. Return loss (S<sub>11</sub>) plots for (a) DMS CSPA (b) SMS CSPA.**

**TABLE III  
DMS CSPA PERFORMANCE PARAMETERS**

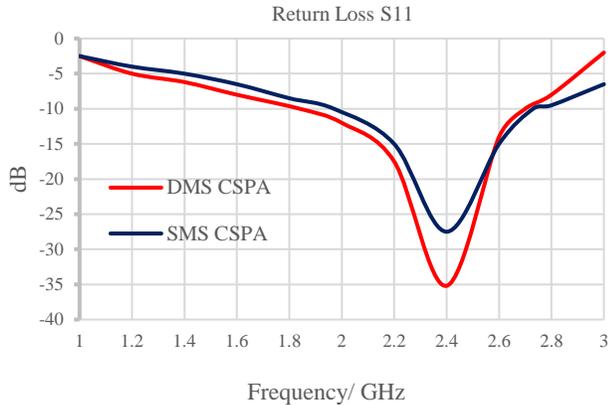
| Parameter                | Value |
|--------------------------|-------|
| Percentage bandwidth (%) | 37.8  |
| Return loss (dB)         | -35.2 |
| Bandwidth (GHz)          | 0.86  |

**TABLE IV  
SMS CSPA PERFORMANCE PARAMETERS**

| Parameter                | Value |
|--------------------------|-------|
| Percentage bandwidth (%) | 32.3  |
| Return loss (dB)         | -27.5 |
| Bandwidth (GHz)          | 0.76  |

#### IV. COMPARATIVE ANALYSIS OF DMS AND SMS CSPA

The effects of substrate combination on microstrip patch antenna performance have been studied and analyzed using two antenna performance parameters (return loss and bandwidth) plot for comparison is presented in Fig.3.



**Fig. 3.** The comparative plot of return loss for DMS CSPA and SMS CSPA.

Figure 3 compares the return loss of the designed DMS CSPA and the SMS CSPA at a resonance frequency of 2.4 GHz. The return loss of the DMS CSPA and the SMS CSPA has been observed as -35.2 dB and -27.5 dB signifying a 7.7 dB difference. Also, a 0.1 GHz difference in bandwidth has been observed in Table III and Table IV. The bandwidth difference between the antennas is a result of the difference in the effective dielectric constants of the antennas presented in Section III; as reported in various microstrip patch antenna literature, lower effective dielectric constants result in increased width of the patch, thus providing a larger bandwidth [29], [30]. So to produce a substrate with a lower effective dielectric constant, a substrate material with a lower dielectric constant is combined with the FR-4 substrate, as shown in Section III. Thus, the combination reduces the effective dielectric constant of FR-4 from 4.3 to 3.9. The reduced effective dielectric constant of combined substrate material increases the bandwidth from 0.76 GHz (1.97 GHz ~ 2.73 GHz) to 0.86 GHz (1.84 GHz ~ 2.7 GHz). Also, when bandwidth increases, the return loss of the microstrip antenna becomes lower; this explains why there is a reduction in return loss from -27.5 dB to -35.2 dB.

Though both antennas presented a good return loss and bandwidth characteristics, the additional 100 MHz bandwidth presented by the DMS CSPA will allow for usage in both integrated design for IEEE 802.11, Wireless Local Area Network(WLAN) standards of 2.4 GHz (2400 MHz ~ 2484 MHz) standards, Worldwide Interoperability for Microwave Access (WiMAX) standards of 2.5 GHz (2.5 GHz ~ 2.69 GHz), and Personal Communication Service (PCS) bands of 1.9 GHz (1850.2 MHz ~ 1989.8 MHz). The DMS antenna can be very useful in Canada, Mexico, and the United States, where the 1.9 GHz

frequency band has been designated by the Industry of Canada and the United States Federal Commission for new wireless services to alleviate capacity caps inherent in the original Advanced Mobile Phone Systems (AMPS) and Digital AMPS (D-AMPS).

#### V. CONCLUSIONS AND FUTURE WORK

Though the two antennas presented have been observed to have good and acceptable values of return loss VSWR and bandwidth, the DMS CSPA displayed a better performance characteristic in comparison with the SMS CSPA. The better bandwidth characteristics presented by the DMS CSPA makes it suitable in integrated design for IEEE 802.11, Wireless Local Area Network(WLAN) standards of 2.4 GHz (2400 MHz ~ 2484 MHz) standards, Worldwide Interoperability for Microwave Access (WiMAX) standards of 2.5 GHz (2.5 GHz ~ 2.69 GHz), and Personal Communication Service (PCS) bands of 1.9 GHz (1850.2 MHz ~ 1989.8 MHz), especially in Canada and United States where the 1.9 GHz band has been allocated for PCS.

As a continuation of this work, physical implementation and comparative analysis of the proposed model will be presented, using gain, directivity radiation efficiency, and radiation pattern as a standard to verify the efficiency and usability of the proposed design in the 5G regime of frequencies.

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