**Original Article** 

# Use of Combined Gas Supply to Increase Thermal Efficiency of Plasma Processes

Sergey Dmitrievich Neulybin

Head of the laboratory, Laboratory of Methods of Creation and Design of Material-Technology-Construction Systems, Perm National Research Polytechnic University, Perm, Russian Federation

**Abstract** — The results of comparative studies of heat transfer to the plasma torch elements and product simulator are presented in this article. The possibility of a significant increase in heat transfer to the product during plasma treatment with a plasma jet by changing the connection diagram of the plasma torch and using a combined supply of plasma and shielding gas is shown.

**Keywords** — *Heat transfer, Plasma arc, Plasma treatment, Plasma torch.* 

# **I. INTRODUCTION**

Controlling heat transfer in the product makes it possible to increase the productivity and quality of plasma processing of metals [1]-[3].

An increase in the heating capacity of the compressed arc due to an increase in the current leads to an increase in heat input into the plasma torch elements that, in its turn, adversely affects the service life of the plasma torch and trouble-free operation in general [4]. In addition, there is a connection between the value of the welding current and geometric parameters of the plasma torch - the diameter and height of the plasma-forming nozzle channel in particular [5]. For each specific geometric parameter, there is a critical current value, and it's exceeding leads to emergency mode [6].

Specific heat content (enthalpy), i.e. the amount of heat contained in a unit of volume or mass of the arc is an important parameter of a compressed arc (Fig. 1). The use of high-enthalpy molecular plasma-forming gases is energetically more profitable since they have the same thermal efficiency as monatomic gases at lower temperatures [7]. At the same time, heat loss due to radiation into the walls of the plasma torch and the environment is reduced. The influence of the plasma-forming gas on plasma arc thermal characteristics has been studied in sufficient detail in previous years [8].

Shielding gases have a great influence on the quality of the welded joint [9]. To ensure quality, it is necessary to use a shielding gas suitable for the material to be processed [10], [11]. In this case, their physical properties such as ionization and dissociation energy, thermal conductivity, atomic mass, and chemical reactivity have critical importance. Inert and active gases, as well as their mixtures, are used as shielding gases [12]-[13].



Inert gases protect the arc and the welded metal without metallurgical influence. Argon, due to its high atomic mass, provides effective protection of the treatment area. It occurs as a result of achieving the large kinetic energy of the plasma jet. Low ionization potential provides high voltage and highfrequency discharge. However, argon has low thermal conductivity and low heat capacity. During welding copper, it is advisable to use nitrogen, because nitrogen is inert concerning copper. In terms of properties (thermal

conductivity, enthalpy, and atomic mass), nitrogen can be

placed between argon and hydrogen. Active shielding gases,

such as carbon dioxide (CO<sub>2</sub>), are mainly used for welding

structural steels because the gas enters into chemical

interaction with the welded metal and dissolves in it. Gas

mixtures have, in some cases, better technological properties

than individual gases. For example, a mixture of argon with carbon dioxide allows alloyed steels to be welded without

burning out the alloying components while reducing spatter

and increasing penetration depth.

	Table 1. 1 locess parameters											
	I, A	dnozzle, mm	Q plasma., l/min	Qshield. , l/min	The polarity of the current							
	50-250	4	3.0	1.7/5.5/7	direct/reve rse							
I					130							

 Table 1. Process parameters

#### **II. METHODS**

The purpose of this work was to study the effect of different shielding gases on the energy parameters of the plasma arc. The studies were carried out in the following order: the heat input into the plasma torch and the product was measured depending on the arc current magnitude and the type and consumption of the shielding gas when operating on a current of direct and reverse polarity. The study of heat input into the plasma torch and the product were carried out by the calorimetry method. Cooling of the plasma torch and the product was implemented using running water. An ESAB LHF-400 power source was used to power the compressed arc with a welding current. Argon (Ar), nitrogen (N<sub>2</sub>), and carbon dioxide (CO<sub>2</sub>) were chosen as shielding gases. The studies were performed with the following model parameters (Table 1).

The arc voltage varies depending on the shielding gas used as shown in Table 2.

Table 2. Arc	voltage changed	
		7

	$\mathrm{U}_\mathrm{EI},\mathrm{V}$							
I, A	Direct polarity			Reverse polarity				
	Ar	$N_2$	$CO_2$	Ar	$N_2$	CO <sub>2</sub>		
50	-	_	21.6	35	31.7	32.9		
100	18	26.2	23	36.3	34.3	36.4		
150	19.5	28	24.2	39.2	35.3	39.1		
180	22.5	29.5	26.3	-	39.7	39.9		

## **III. RESULTS**

When operating in argon at reverse polarity current, the arc voltage increases by about 2 times as compared to operating at direct polarity, and the electric power of the arc also increases accordingly (Table 2).

The measurement results are summarized in graphs of the dependence of heat input into the product on the current.



Fig. 2 Dependence of heat input into the product on the current when operating on direct polarity

When operating at direct polarity current, the greatest heat input into the workpiece, other conditions being equal, is achieved when nitrogen is used as a shielding gas. In the area of the high current, the heat input into the product is more than doubled in comparison with argon (Fig. 2).



Fig. 3 Dependence of heat input into the plasma torch on the current when operating on direct polarity

When using carbon dioxide, the plasma torch carries the least heat load, but the heat input into the product also decreases (Fig. 3).



Fig. 4 Dependence of heat input into the product on the current when operating on reverse polarity

The use of nitrogen and carbon dioxide makes it possible to increase the heat input into the product in high currents area by about 1.7 times in comparison with argon (Fig. 4).



Fig. 5 Dependence of heat input into the plasma torch on the current when operating on reverse polarity

When the plasma torch operates at a current of reverse polarity in low currents area, when all types of shielding gases are used, the plasma torch carries a similar thermal load. However, in high currents area, when carbon dioxide is used, a decrease in heat input to the plasma torch by about 1.5 times is observed (Fig. 5).

### VI. CONCLUSION

- It was found that when operating at reverse polarity current, all other conditions being equal, the heat input into the product increases by about 1.3 1.5 times, however, an increase in thermal load on the plasma torch reduces the efficiency of the process.
- With the same arc current, the highest arc voltage is achieved when using nitrogen as a shielding gas, this affects the electric power of the arc, and therefore the thermal power. The lowest voltage is achieved when argon is used as shielding gas.
- When using high-enthalpy gases nitrogen and carbon dioxide, the heat input into the plasma torch is reduced by 1.2-1.5 times.
- The use of a combined supply of shielding and plasmaforming gas, with constant energy consumption, makes it possible to increase the thermal efficiency of the process, however, the technological features of plasma treatment of certain groups of materials, in particular aluminum and titanium alloys, should be considered. When processing such materials, one hundred percent shielding gas is required and therefore using of an inert gas (argon). During operation at reverse polarity, nitrogen and carbon dioxide, unlike argon, do not provide the proper effect of cathodic cleaning of the processed surface.

# ACKNOWLEDGMENT

The study was supported by the Russian Science Foundation grant No. 21-79-00237, and the Ministry of Science and Higher Education of the Russian Federation (State Assignment of Work No. FSNM-2020-0028), within the national project "Science and Universities" and the State Assignment of Work "Development of Scientific and Technological Foundations for the Formation of a Material-Structure System with Special Properties Based on Hybrid Additive Technologies".

### REFERENCES

- K. Draou, N. Bellakhal, B. G. Chéron, and J. L. Brisset, Heat transfer to Metals in Low-Pressure Oxygen Plasma: Application to Oxidation of the 90Cu–10Zn Alloy, Materials Chemistry, and Physics. 58(3) (1999) 212-220. www.doi.org/10.1016/S0254-0584(98)00268-5
- [2] M. Zhao, Y. Wang, Sh. Yang, J. Li, W. Liu, and Zh. Song, Flow Behavior and Heat Transfer of Molten Steel in a Two-Strand Tundish Heated by Plasma, Journal of Materials Research and Technology. 13 (2021) 561-572. www.doi.org/10.1016/j.jmrt.2021.04.069
- [3] M. Q. Yuan, Y. Zhang, Sh. H. Yang, and H. L. Yi, Active Control of the Near-Field Radiative Heat Transfer Between Two Metal Plates through the External Electric Field, International Journal of Thermal Sciences. 171 (2022) 107208. www.doi.org/10.1016/j.ijthermalsci.2021.107208
- [4] H. Gui, K. Zhang, D. Li, and Zh. Li, Effect of Relative Position in Low-Power Pulsed-Laser–Tungsten-Inert-Gas Hybrid Welding on Laser-Arc Interaction, Journal of Manufacturing Processes. 36 (2018) 426-433. www.doi.org/10.1016/j.jmapro.2018.10.045
- [5] R. Kawalkar, H. K. Dubey, and S. P. Lokhande, Wire Arc Additive Manufacturing: A Brief Review on Advancements in Addressing Industrial Challenges Incurred with Processing Metallic Alloys, Materials Today: Proceedings. 50(5) (2022) 1971-1978. www.doi.org/10.1016/j.matpr.2021.09.329
- [6] Yu. D. Shchitsyn, Plasma Technologies in Welding Production, Part 1, Perm, Russia: Perm State Technical University. (2004) 73.
- [7] V. A. Malakhovskiy, Plasma Processesi in Welding Production, Moscow, Russia: Higher school. (1988).

- [8] A. F. Puzryakov, Theoretical Foundations of Plasma Spraying Technology, Moscow, Russia: Publishing House of MSTU IM, N.E. Bauman. (2008) 358.
- [9] Z. Liu, Ch. Fan, Zh. Ming, Ch. Chen, Ch. Yang, S. Lin, and L. Wang, Optimization of Shielding Gas Composition in High Nitrogen Stainless Steel Gas Metal Arc Welding, Journal of Manufacturing Processes. 58 (2020) 19-29. www.doi.org/10.1016/j.jmapro.2020.08.001
- [10] S. K. Wu, K. Zheng, J. L. Zou, F. Jiang, and X. H. Han, A Study of the Behavior and Effects of Nitrogen Take-Up from Protective Gas Shielding in Laser Welding of Stainless Steel, Journal of Manufacturing Processes. 34(A) (2018) 477-485. www.doi.org/10.1016/j.jmapro.2018.06.031
- [11] Ch. Cai, Sh. He, H. Chen, and W. Zhang, The Influences of Ar-He Shielding Gas Mixture on Welding Characteristics of Fiber Laser-MIG Hybrid Welding of Aluminum Alloy, Optics & Laser Technology. 113 (2019) 37-45. www.doi.org/10.1016/j.optlastec.2018.12.011
- [12] V. A. M. Cristino, P. A. R. Rosa, and P. A. F. Martins Cutting Underactive and Inert Gas Shields: A Contribution to the Mechanics of Chip Flow, International Journal of Machine Tools and Manufacture. 50(10) (2010) 892-900. www.doi.org/10.1016/j.ijmachtools.2010.06.003
- [13] S. Roy, B. Silwal, A. Nycz, M. Noakes, E. Cakmak, P. Nandwana, and Y. Yamamoto, Investigating the Effect of Different Shielding Gas Mixtures on Microstructure and Mechanical Properties of 410 Stainless Steel Fabricated Via Large Scale Additive Manufacturing, Additive Manufacturing. 38 (2021) 101821. www.doi.org/10.1016/j.addma.2020.101821